

# Novel Approach Of Microstrip tri-Band Bandpass Filter for GSM, Wimax And UWB Application

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## Abstract

*In this paper, a novel approach of miniature tri-band microstrip bandpass filter is design for the application of GSM(1.8GHz), WiMAX(3.4GHz) and UWB(6.5-8.1GHz) using Asymmetric SIRs and DGS to achieved the basic characteristic of microstrip filter such as low insertion loss, high selectivity, wider range of bandwidth, low group delay. The novel filter is design intentionally selecting the impedance ration(R) and length of the microstrip of the asymmetric SIRs and DGS is used to improve the coupling strength of the desired band. The measurement entities of the novel filter for GSM (1.8GHz), WiMAX (3.4GHz), and UWB (6.5-8.1GHz) are insertion losses ( $S_{21}$ ) are -0.07dB/-0.21dB/-0.12dB, and return losses ( $S_{11}$ ) are -31dB/15dB/30dB respectively. The response of the filter was simulated using An soft HFSS Simulator.*

## Keywords

*BPF, WiMAX, UWB, Asymmetric SIRs, DGS, FBW.*

## 1. INTRODUCTION

Miniature and selective required resonance frequency pass bands from the wider range of frequencies are the major attraction in the wireless communication systems [1]. To constitute the multi-band in a single system in the electronic devices and filter unwanted frequencies abstract is more interest in Modern microwave filter design Techniques [2-3]. Therefore multi-band filter obtain a great interest from last few decades in modern wireless communication system. Microstrip multi-band filter can easily fabricate and integrated on dielectric substrate and providing high design freedom during exact measurement of width, length and thickness of the microstrip lines [4]. The multi-band Bandpass filter is design in many authors, but still it is large circuit area and high design complexity which are not fruitful for wireless communication systems where miniaturization is most vital issue now-a-days in the miniaturize Bandpass filter design methods [5]. In RF and microwave communication devices, in wireless communication systems multiple service Bandpass filters are carry out more and more interest and aggressively developed and design. In radio frequency front end, Bandpass filter plays a key role for selecting the desired band and attenuated the unwanted band from the signals. A tri-band microstrip BPF was proposed to realize with compact size, low return loss and wide band characteristics that is discuss details in [6].

In microstrip filter design, Stepped impedance resonators is widely used to design Bandpass filter because of compact in size, low insertion loss, proper coupling flexibility, high design freedom of selecting the electric length ratio ( $\mu$ ) and impedance ratio (R) in the desired filter to achieved the desired band [8-9]. A new methods of design to improve the response in Bandpass filter and

increases the bandwidth allocation in the passband response, defected SIRs, using the DGS [10]. Stepped impedance resonators are also used to acquire UWB response by controlling the resonance frequencies in closed and configuring the strong coupling on side the resonators [11]. UWB filter were design using the SIRs and a DGS by combining of wide band and rejected notch-band [12-14].

In this paper, novel ways of designing the tri-band microstrip bandpass filter using one pair of Asymmetric SIRs and DGS. We obtain three centre frequency band 1.8GHz, 3.4GHz and 6.5-8.10GHz by intelligently selecting the impedance ratio( $R$ ) and electrical length ratio ( $\mu$ ) of the proposed filter SIRs and DGS. Obtained the tri-band response by integrated the two narrow passband with wideband response [15].

## 2. DESIGN METHODOLOGY

The coupling scheme is shown in fig. 1 of the proposed Bandpass filter. The proposed filter layout is shown in the Fig. 2. Basically the BPF consisting one pair of Asymmetric SIRs and a DGS on ground plane and couple of Input/output microstrips line. Firstly two narrow passband are design using two Asymmetric SIRs to obtain the centre frequency 1.8GHz and 3.4GHz for the application of GSM (1.8GHz), WiMAX (3.4GHz) and UWB (6.5-8.1GHz). The last passband is design by using the defected ground structure on the ground plane with microstrip line to get the ultra-wideband frequency response. The DGS is arrange under the ground plane of the symmetrically to avoid the design complexity and reduces the compensation. If the electrical length ratio and impedance ratio are different the DGS will be affected the other resonator modes of asymmetric SIRs. Finally by integrated the tri-bands response is obtained that is reported in the observation part. The passband are obtain form the resonator 1 and resonator 2 and the second passband are form the resonators 3 and resonators 4. The last band are measure form the resonators 1,3,4 and 2.

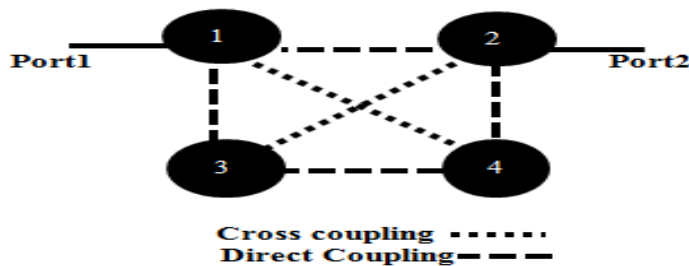


Fig1. Coupling Scheme Of The Proposed Filter.

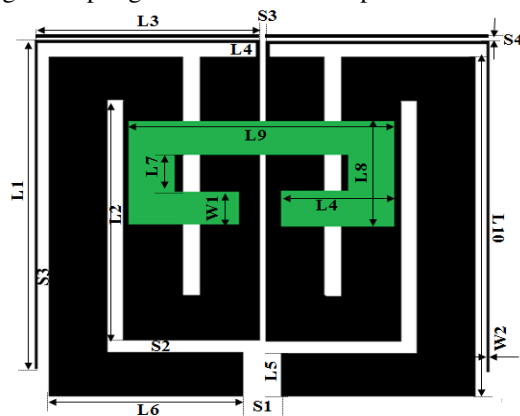


Fig2. The Proposed Filter Layout.

It was known that DGS under the coupling resonators can be seen as a parallel LC resonator [20]; the capacitance and the inductance are calculate using (1) and (2)

$$C = \frac{\omega_c}{Z_0 g} \cdot \frac{1}{\omega_0^2 - \omega_c^2} \quad (1)$$

$$L = \frac{1}{4 \pi^2 f_0^2 C} \quad (2)$$

Where  $\omega_c$ ,  $\omega_0$  is the cut-off frequency and Centre frequency of the low-pass filter,  $Z_0$  the Characteristic impedance of the input/output ports, and ‘g’ given by the element value of the prototype Low Pass Filter. The operating frequency of DGS can be lowered while the reactance is increased by generally increasing the area or the number of DGSs. The centre frequency and the relative fractional bandwidth (FBW) can be measure by the following equation

$$\omega_0 = \sqrt{\omega_1 \omega_2} \quad (3)$$

$$FBW = \frac{\omega_2 - \omega_1}{\omega_0} \quad (4)$$

### 3. SIMULATION RESULT DISCUSSIONS

Based on design structure as shown in the fig. 2 the response of the proposed filter and their S-parameters is depicted in fig. 3. The magnitude of  $S_{11}$  and  $S_{21}$  vs. frequency plot at the centre frequency 1.8/3.4/6.5-8.1 (GHz) responses and the phase difference of transmission are shown in fig.3. The insertion losses ( $S_{21}$ ) are very low those are -0.07dB/-0.21dB/-0.12dB and the return losses ( $S_{11}$ ) are --31dB/-15dB/-30dB for the GSM (1.8GHz), WiMAX (3.4GHz) and UWB (6.5-8.1GHz) respectively. The appearing of transmission zeros at the end of the each side of the passband improved the selectivity that is shown in the fig. 3 and Fig.5 and it are granted the sharpness of the scattering parameters of the design filter response. The minimum transmission zero is -77dB at the frequency (1.15GHz) and the maximum is -50dB (8.23GHz). The appearance of two transmission poles at each passband at the last two band increases the 3dB bandwidth as shown in Fig. 3 and Fig. 4. The group delay is calculating by taking the derivative of phase, which is inversely proportional to bandwidth as shown in Fig.6. The Group delay for GSM (1.8GHz), WiMAX (3.4GHz) and UWB that are 5 ns at 1.8GHz and 0.12 ns at 3.4GHz and 2.5ns at (6.5-8.1GHz) which are shown in the fig. 6. In this design, the group delay for GSM (1.8GHz), WiMAX (3.4GHz) and UWB are good and applicable.

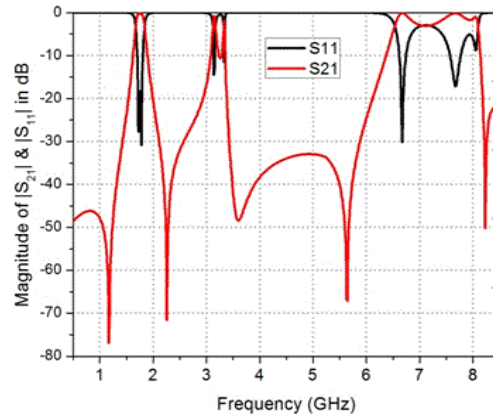


Fig3.  $S_{21}$  and  $S_{11}$  vs. Frequency Plot.

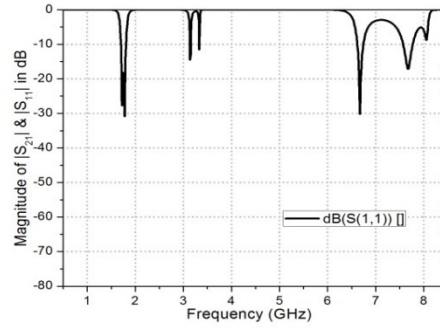


Fig4.  $S_{11}$  Vs. Frequency Plot.

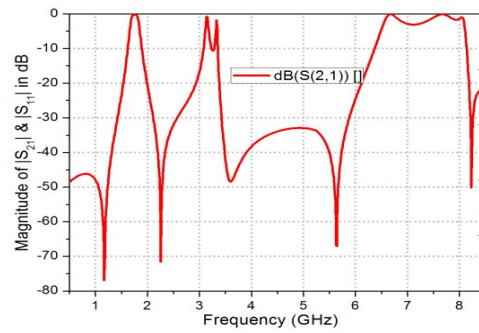


Fig5.  $S_{21}$  Vs. Frequency Plot.

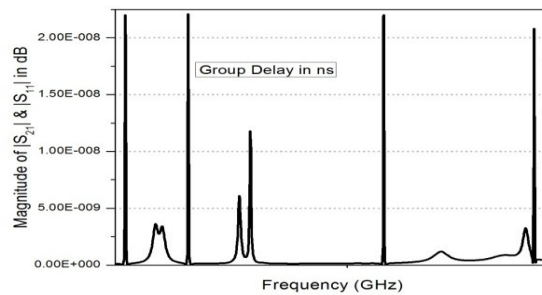


Fig6. Group Delay (Ns) Vs. Frequency Plot

The Fractional Bandwidth (FBW) Of The Proposed Filter Is Measure Using Ansoft HFSS Simulator. The FBW Is 9.77%/2.22%/22.03 With Centre Frequency 1.8ghz, 3.4ghz And UWB (6.5-8.10GHZ) Respectively.

#### 4. DIMENSION CALCULATION AND COMPARISON OF RESULT

The proposed filter was simulated using the Ansoft HFSS Simulator design on a Rogers RT/Duriod 5880 substrate with thickness of 0.787mm, dielectric constant ( $\epsilon_r$ ) of 2.2 and tangent loss ( $\delta$ ) 0.0009. The filter achieves a high impedance ( $Z_1=66.2\Omega$ ) with strip width 0.2mm and low impedance is ( $Z_2=47.17\Omega$ ) with strip width 3.85mm. The dimension of the proposed filter are  $L_1=14.65\text{mm}$ ,  $L_2=10.55\text{mm}$ ,  $L_3=7.45\text{mm}$ ,  $L_4=3.7\text{mm}$ ,  $L_5=2\text{mm}$ ,  $L_6=6.5\text{mm}$ ,  $L_7=16\text{mm}$ ,  $L_8=4.6\text{mm}$ ,  $L_9=8.8\text{mm}$ ,  $L_{10}=15.05\text{mm}$ ;  $S_1=1.2\text{mm}$ ,  $S_2=0.2\text{mm}$ ,  $S_3=0.5\text{mm}$ ,  $S_4=0.1\text{mm}$ ,  $W_1=1.5\text{mm}$ ,  $W_2=0.2\text{mm}$ , with microstrip width of 0.2mm. The complete in size of the proposed filter is  $(17 \times 15) \text{mm}^2$  which is very compact in size compared to other traditional design filters. It is reported that the proposed filter adequate very loss insertion loss, even when the strip width is high (3.87mm). The performance improvement comparisons with previous work are reported in the table 1.

Table 1. Comparison with Other Proposed Tri-Band Bpf

Comparison of model	1 <sup>st</sup> /2 <sup>nd</sup> / 3 <sup>rd</sup> Pass-band (GHz)	$ S_{21} _{\text{lin}}$ dB	$ S_{11} _{\text{lin}}$ dB	FWB (%)	Dimension	Application
Ref.[16]	1/2.5/3.6	2.2/1.8/1.7	20/40/35	5/2.1/1.4	60x60	GSM WiMAX WLAN
Ref.[17]	1/2.5/3.6	2.2/1.9/1.7	15/35/20	5/2.5/1.4	40x40	GSM WiMAX WLAN
Ref.[18]	2.5/3.5/5.9	2.1/1.9/2.3	18/30/22	3.5/3.8/4.5	60x60	WiMAX WiMAX WLAN
Ref.[19]	1.5/2.4/3.5	1.6/1.5/2.3	9/18/13.7	5.2/3.8/4.6	49x56.2	GSM WLAN WiMAX
Propose filter	1.8/3.4/ 6.5-8.1	0.07/0.21/0.1 2	31/15/30	9.77/2.22/22.0 3	17x15	GSM WiMAX UWB

#### 5. CONCLUSION

The new tri-band microstrip bandpass filter is proposed to achieved three passbands at the centre frequency 1.8/3.4/ (6.5-8.10) GHz for the application of GSM (1.8), WiMAX (3.4) and UWB (6.5-8.1) GHz. This filter has advantage that by controlling the resonators modes of the asymmetric SIRs of the proposed filter three bands can be tune. This is generally achieved by selecting the R and  $\mu$  that is describe in introduction part. The filter configurations are with the asymmetric stepped impedance resonators and DGS in ground plane is arranging under the asymmetric SIRs and RT Duriod dielectric substrate. The propose multi-band bandpass filter of the last two passband produces the two transmission zeros at each, which evidence that selectivity of the filter is increases. From the table.1 it is also evidence that circuit size of the propose filter

greatly reduces about 70% than the other filter that are reported in this paper and 3dB bandwidth is also increases compare to the other tri-band filters. The basic characteristic of the propose filter are insertion loss ( $S_{21}$ ) are -0.07dB/-0.21dB/-0.12dB and the return losses ( $S_{11}$ ) are -31dB/-15dB/-30dB for the Centre frequency 1.8/3.4/6.5-8.10 (GHz) respectively. So from the above characteristic of the propose filter it is aspect that it is applicable in microwave integrated circuits, with high performance in the Radio frequency front-end, while wide range of attenuation bandwidth which makes it enables for the application of microwave communication, satellite and wireless communication systems and small cellular base station which are very demanding field in the communication systems.

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